

# Noise is a powerful tool ... From CM ... medicine...to financial markets

## Direct Observation of a Fractional Charge

R. de-Picciotto, M. Reznikov, M. Heiblum, V. Umansky, G. Bunin and D. Mahalu

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Ever since Milliken's<sup>1</sup> famous experiment it is well known that the electrical charge is quantized in units of the electronic charge -  $e$ . For that reason, Laughlin's<sup>2</sup> theoretical prediction of the existence of fractionally charged *quasi particles*, put forward in order to explain the *Fractional Quantum Hall* (FQH) effect, is very counter intuitive. The FQH effect is a phenomenon that occurs in a *Two Dimensional Electron Gas* (2DEG) subjected to a strong perpendicular magnetic field. This effect results from the strong interaction among the electrons and consequently current is carried by the above mentioned *quasi particles*. We directly observed this elusive fractional charge by utilizing a measurement of *quantum shot noise*. *Quantum shot noise* results from the discreteness of the current carrying charges and thus is proportional to their charge,  $Q$ , and to the average current  $I$ , namely,  $S_I=2QI$ . Our *quantum shot noise* measurements unambiguously show that current in a 2DEG in the FQH regime, at a *fractional filling factor*  $\nu=1/3$ , is carried by fractional charge portions  $e/3$ ; in agreement with Laughlin's prediction.

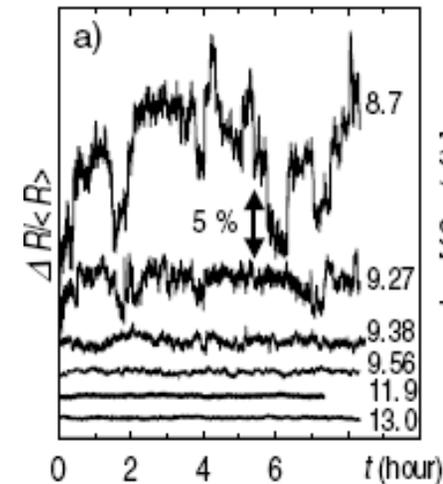
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PHYSICAL REVIEW LETTERS

30 DECEMBER 2002

## Universal Behavior of the Resistance Noise across the Metal-Insulator Transition in Silicon Inversion Layers

J. Jaroszyński,<sup>1,\*</sup> Dragana Popović,<sup>1</sup> and T.M. Klapwijk<sup>2</sup>



VOLUME 70, NUMBER 9

PHYSICAL REVIEW LETTERS

1 MARCH 1993

## Long-Range Anticorrelations and Non-Gaussian Behavior of the Heartbeat

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(Received 15 October 1992)

We find that the successive increments in the cardiac beat-to-beat intervals of healthy subjects display scale-invariant, long-range anticorrelations (up to  $10^4$  heart beats). Furthermore, we find that the histogram for the heartbeat intervals increments is well described by a Lévy stable distribution. For a group of subjects with severe heart disease, we find that the distribution is unchanged, but the long-range correlations vanish. Therefore, the different scaling behavior in health and disease must relate to the underlying dynamics of the heartbeat.

PACS numbers: 87.10.+e

## DETRENDED FLUCTUATION ANALYSIS OF THE FOREIGN EXCHANGE MARKET

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# Noise and grounding issues

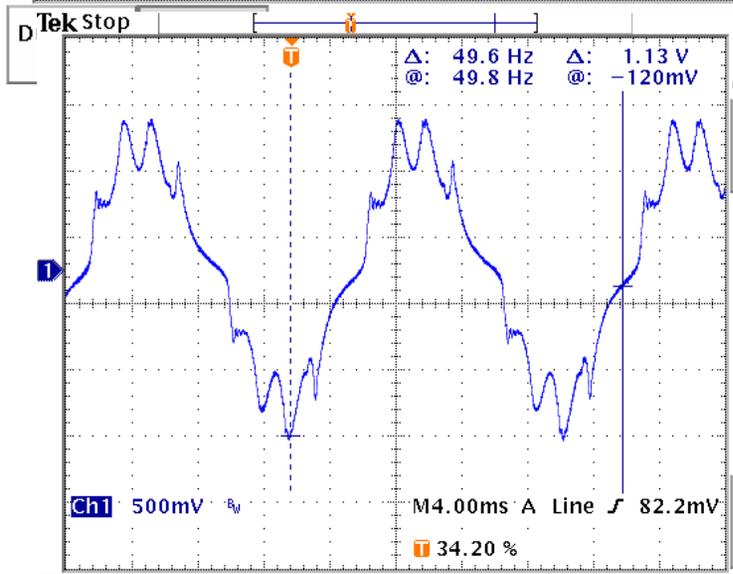
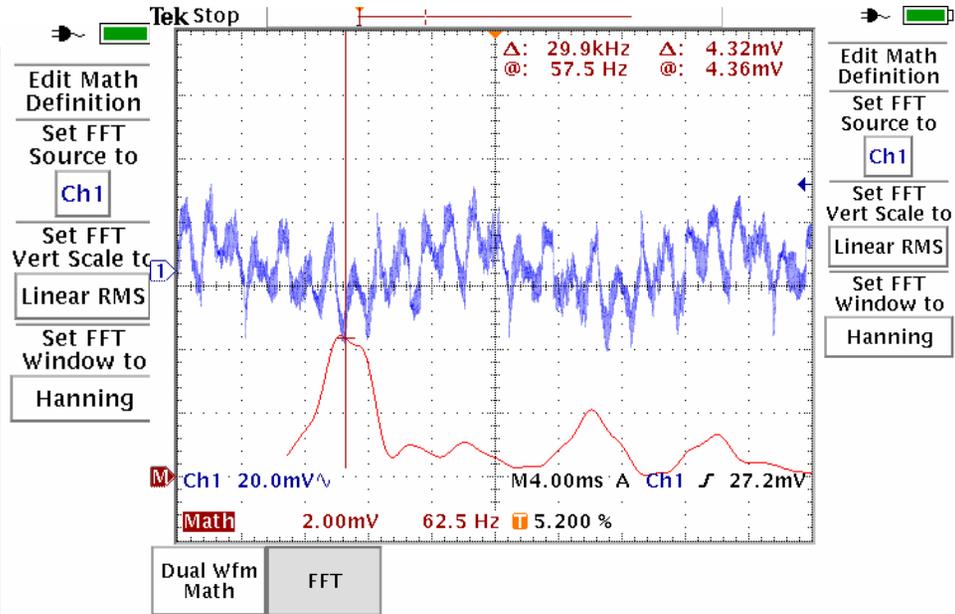
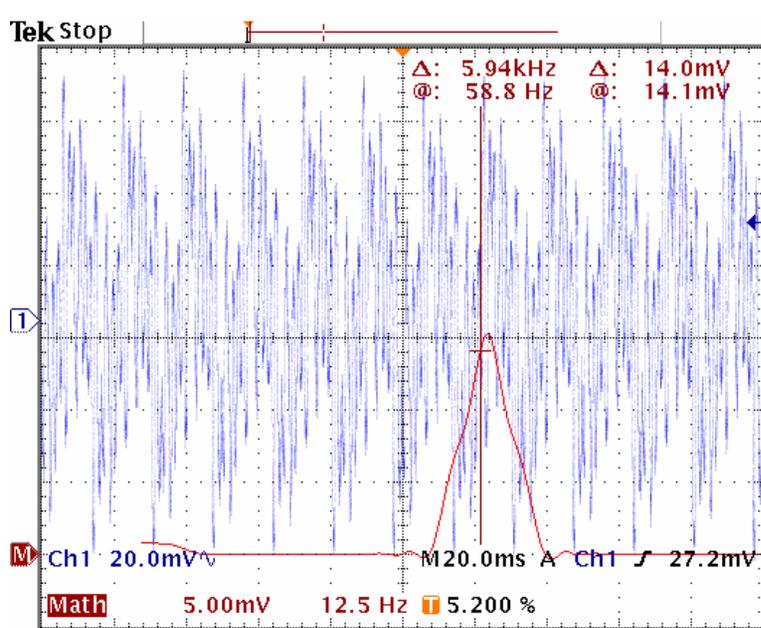
Noise team:

B.L. Brandt, L.W. Engel, S.T. Hannahs, J.J. Jaroszynski, A. Migliori,  
T.P. Murphy, E.C. Palm, D. Popovic, A. P. Reyes, A. Souslov

# Outline

- Sources of low frequency noise
- Existing grounding system
- New grounding system
- High frequency problems
- Diagnostic methods
- How to increase signal/noise ratio
- Examples of improvement
- Plans for further improvements

# At lower frequencies, here is what we are up against



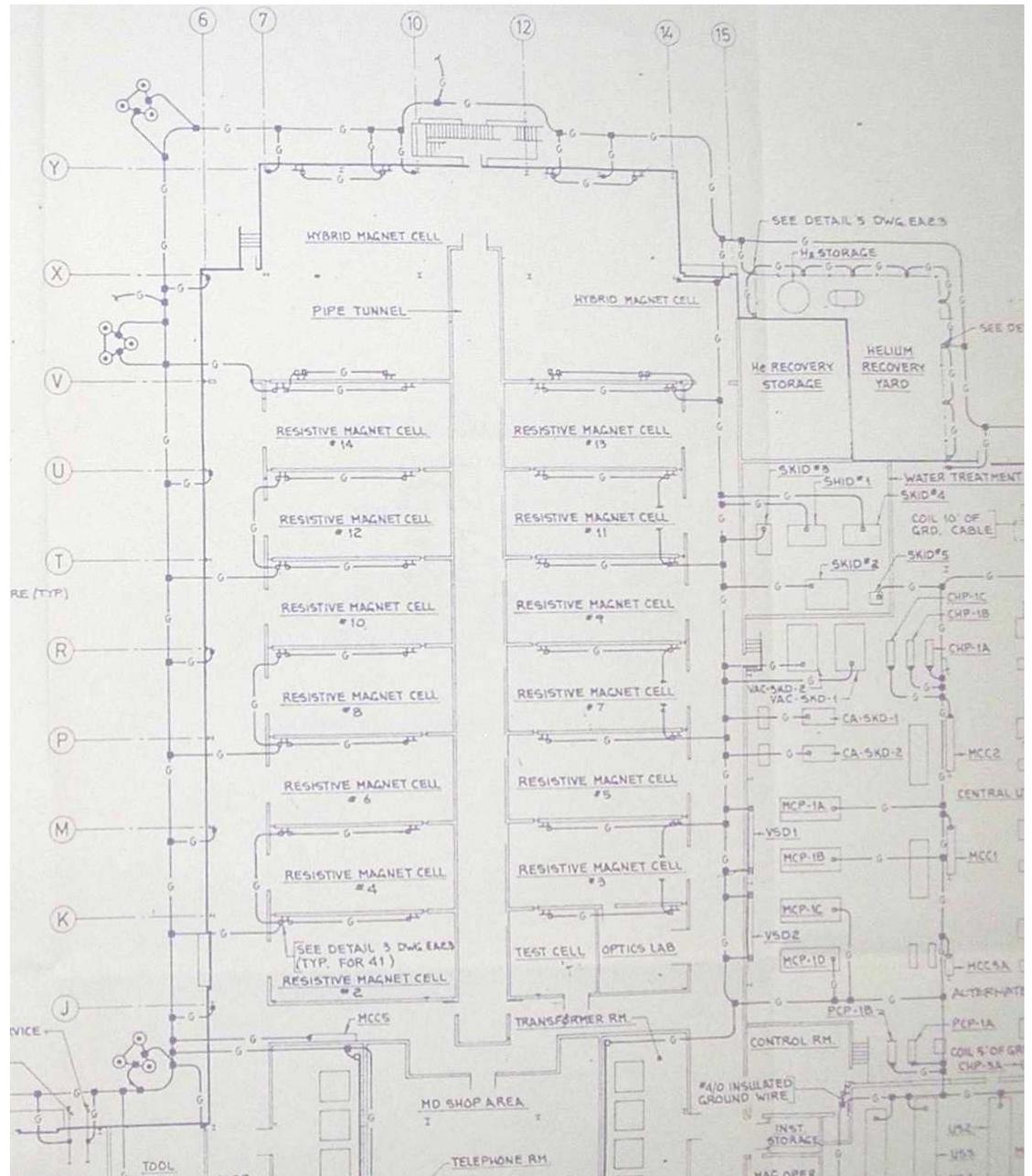
In the air-radiated

On the ground

higher voltages than excitation on the samples, thermometers

# Existing grounding system:

- existing grounding system is interconnected between magnets, cells, power outlets water mains, building construction
- this makes it a huge net which picks-up a lot of noise:  
currents up to 1 A,  
voltages up to 1 V



# Existing grounding system:

AC currents in grounding cables  
When DC power supply on  
Only hybrid was operated at B=24 T



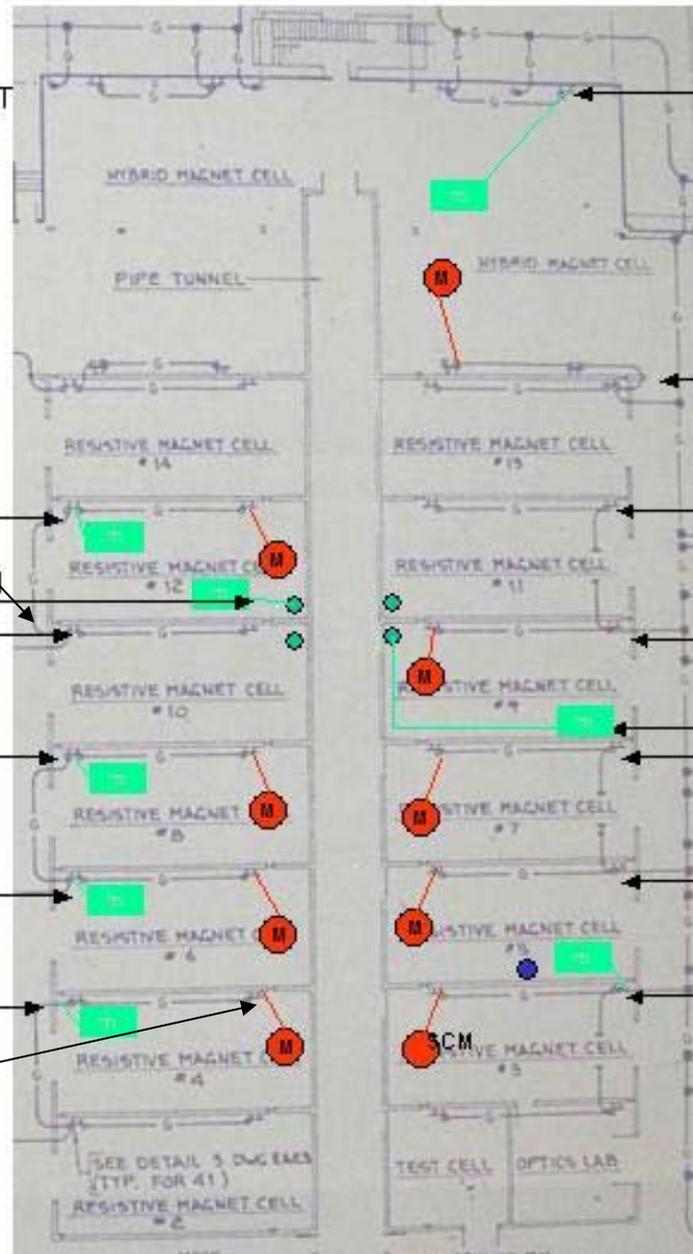
25mA @60Hz  
< 1 mA when on this separate ground

25/ 3 mA @60Hz

140mA @60Hz

600mA @60Hz

40mA @60Hz



4mA @120Hz  
< 1 mA GPIB separated

40mA @60Hz

Nothing connected, very clean

40mA @60Hz

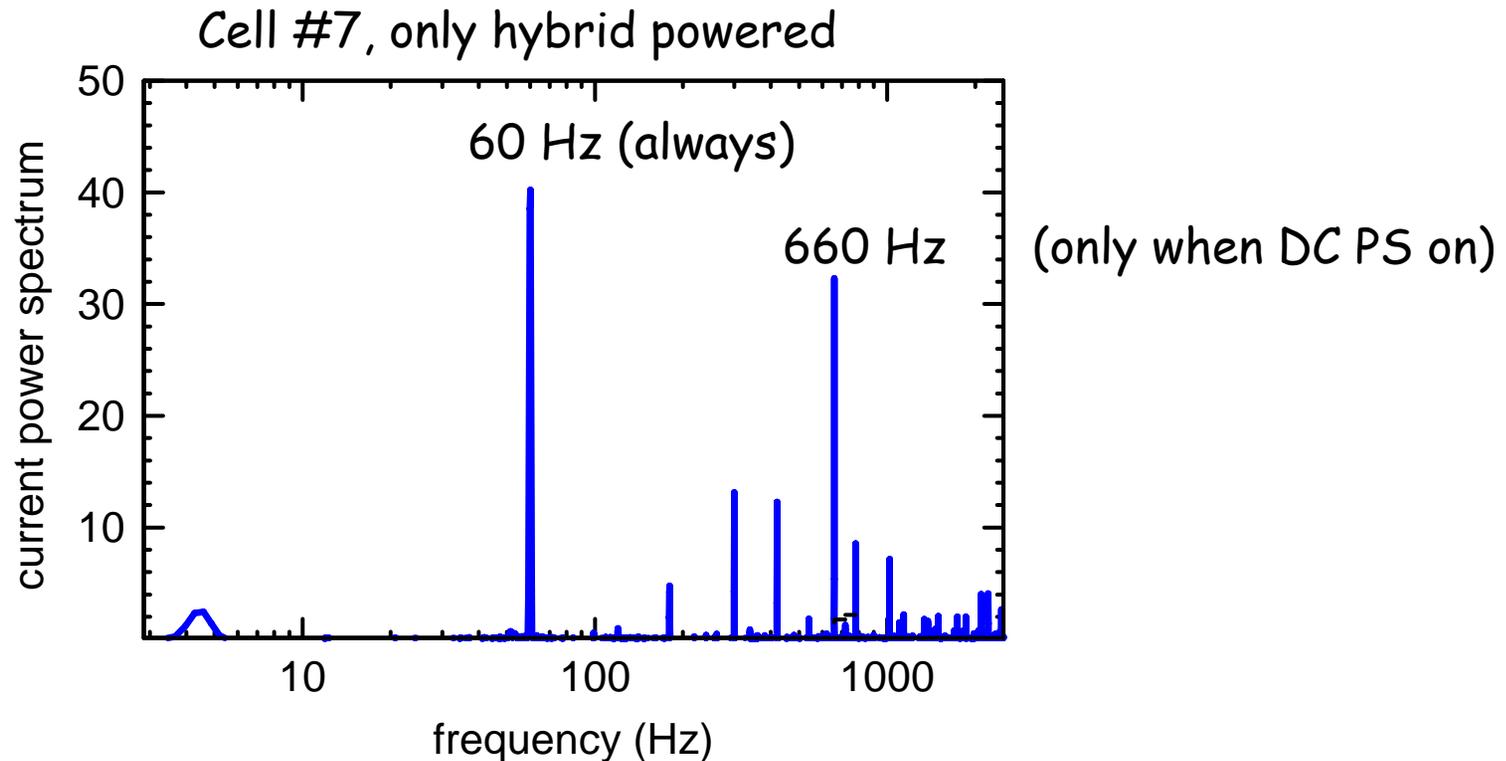
3mA @660Hz

50mA @60Hz, 40 mA@660

50mA @60Hz, 40 mA@660

4mA @180Hz

Typical spectrum of the noise in grounding cables in cells #2-14  
when switching DC power supply is on



set your frequency  $f < 60$  Hz or  $f > 3$  kHz:

Johnson noise (nV) from 1 kOhm resistor could be measured here

avoid especially 200Hz - 2 kHz

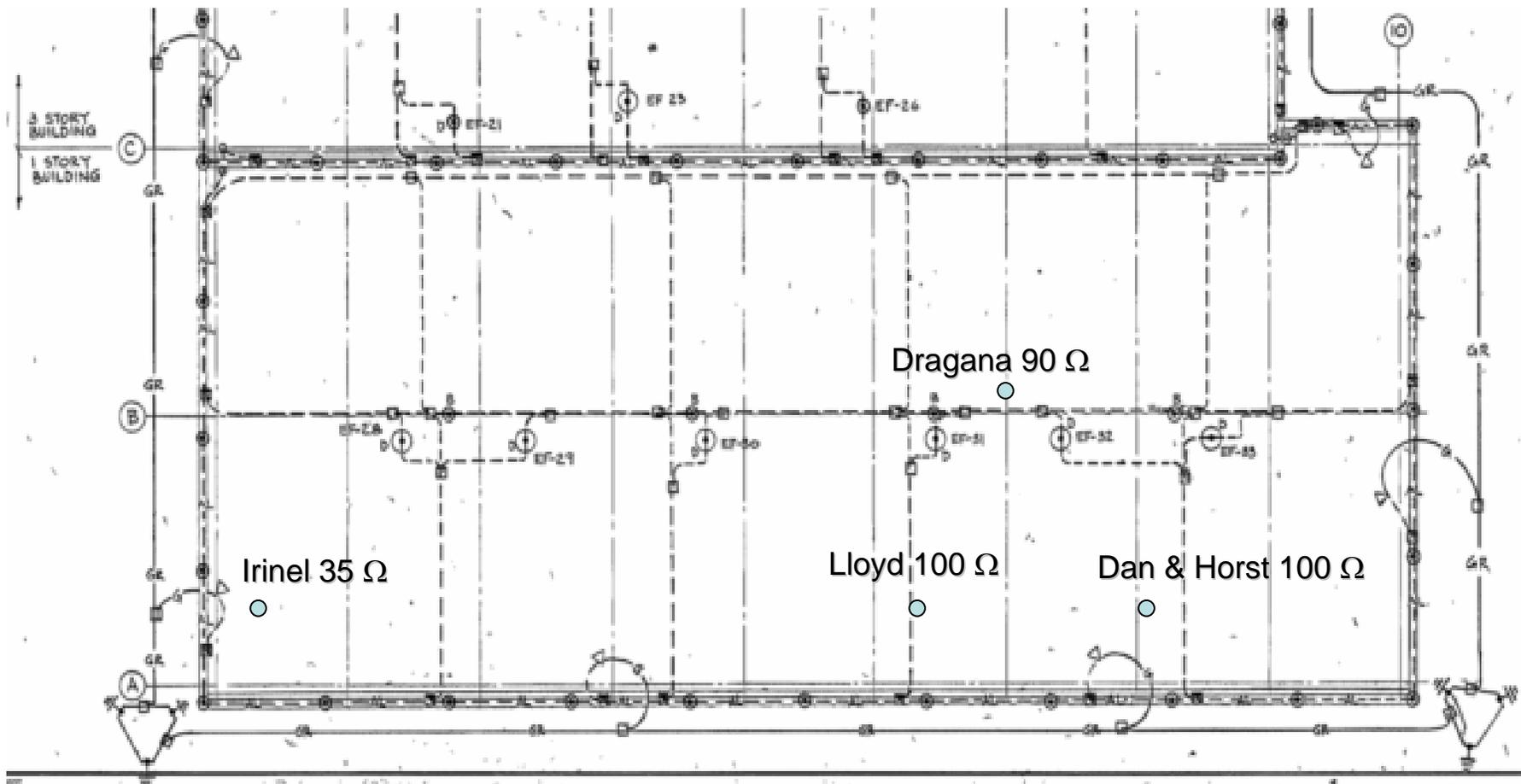
users from Europe: be aware of 60Hz, not 50 Hz

new power supply will be installed soon

# It is not easy to make a good ground in Florida soil:

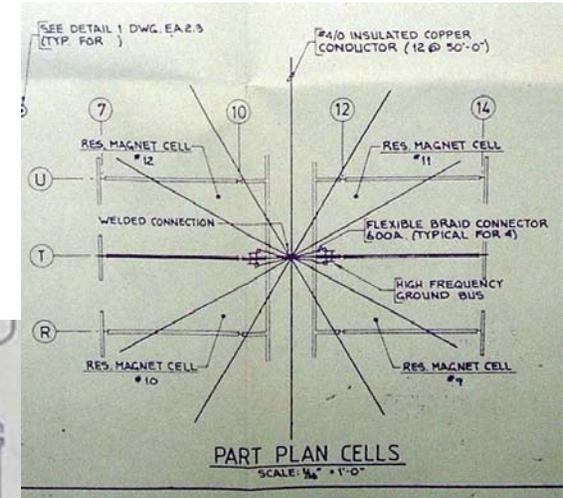
Grounding rods in C120 measured with 3 probe method vs. the racetrack  
@575 Hz, 2 days after 1 in of rain and 2 months of drought in April  
Now: 50% more

**Safety: maximum 25  $\Omega$  !!!**

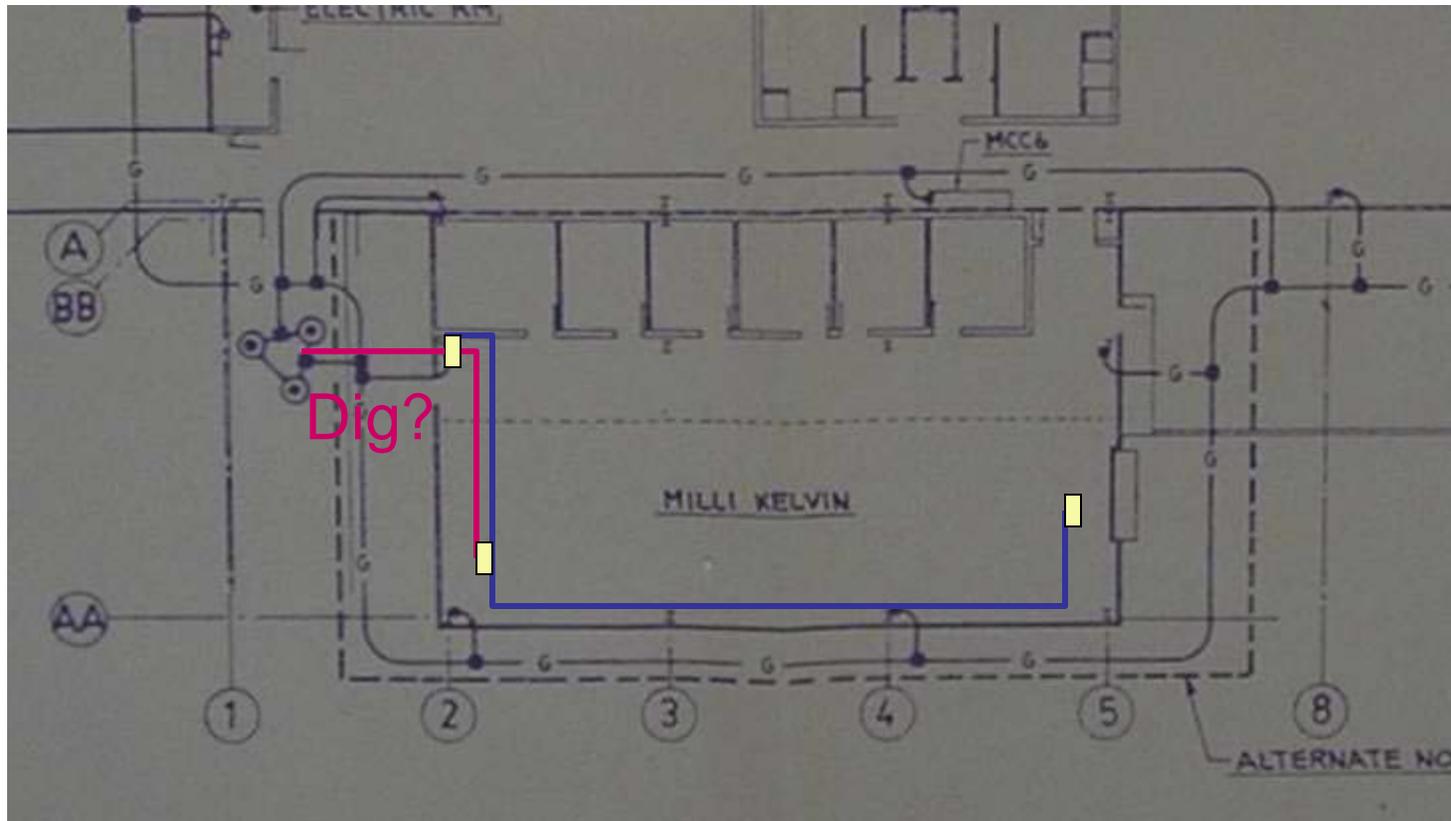


New grounding system (almost done)  
flat festoon cables extended from star  
ground in cells #9-12  
these cables have reduced inductance

any cable has approx.  $1 \mu\text{H}$  per meter!!!



# Millikelvin building:



# New grounding bars:

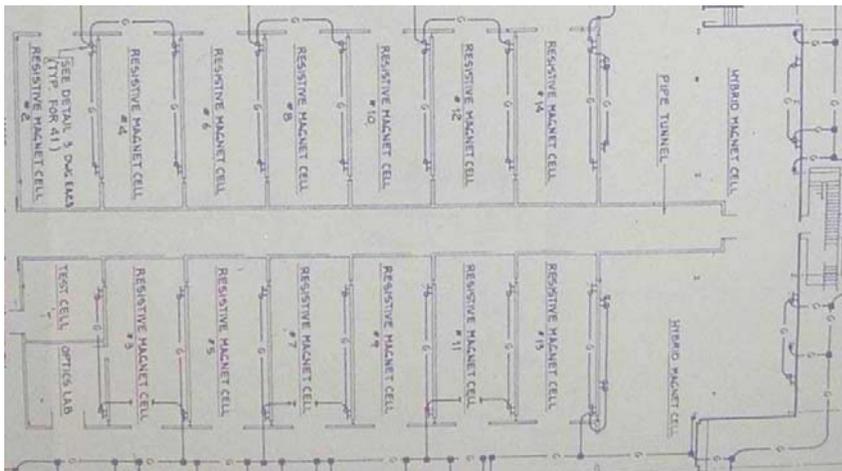


It is absolutely critical not to connect it to any other grounding  
It could spoil your experiment as well as experiment in other cells !!!

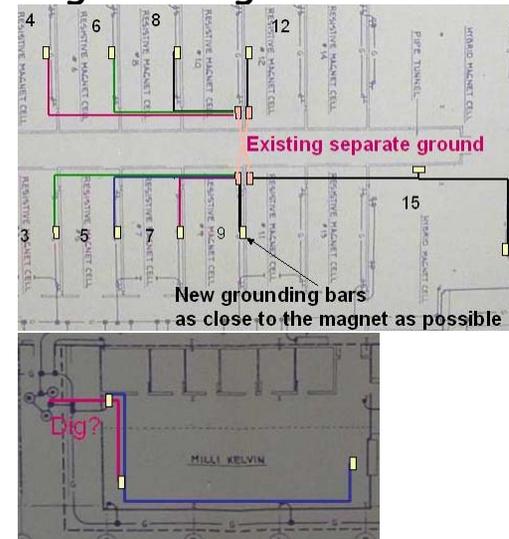


# Grounding issues

- existing grounding system is interconnected between magnets, cells, power outlets water mains, building construction
- this makes it a huge net which pick-up a lot of noise: currents up to 1 A, voltages up to 1 V

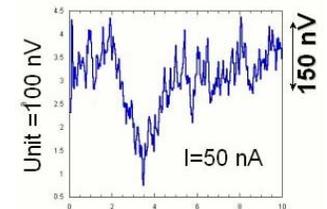


- alternate solution: to extend "forgotten" star ground from cells #9,10,11,12 to other cells (work almost done)
- using flat festoon cable 4x4 AWG
- it has resistance as 3/0 welding cable but lower inductance,
- in millikelvin building: connect ground directly to grounding rods



- solution: to separate ground in each cell
- however, measurements show that existing home made grounding rods have high resistance: 15-140 Ohm after 2 month of drought, while the most liberal US safety norm is 25 Ohm.
- it is also not easy to drill trough 2' concrete platform

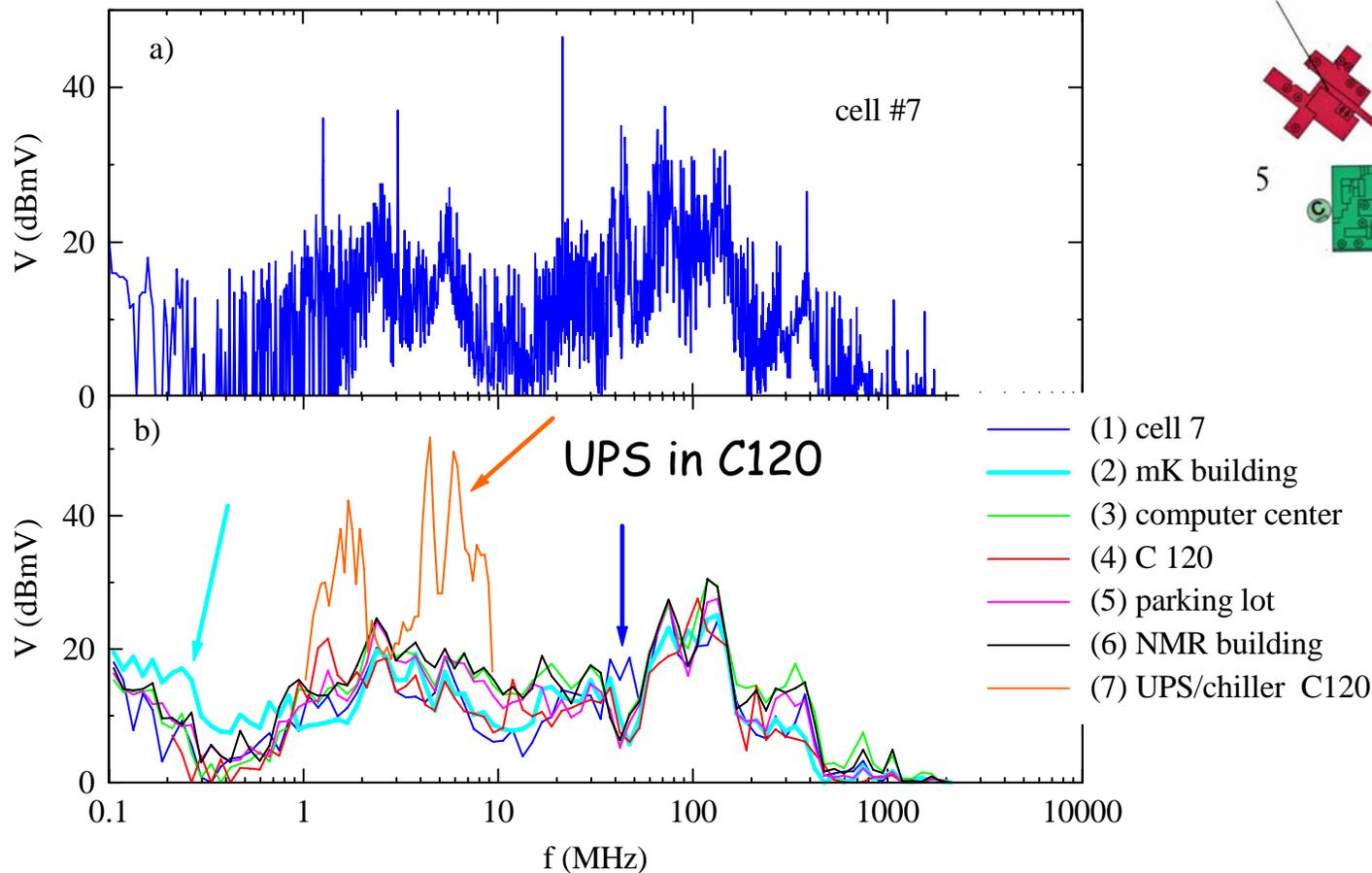
- importance of good grounding: after "cleaner" grounding point found, resistive detection of NMR in FQHE regime is possible in the hybrid (Jiang&Stormer)



# High frequency problems:

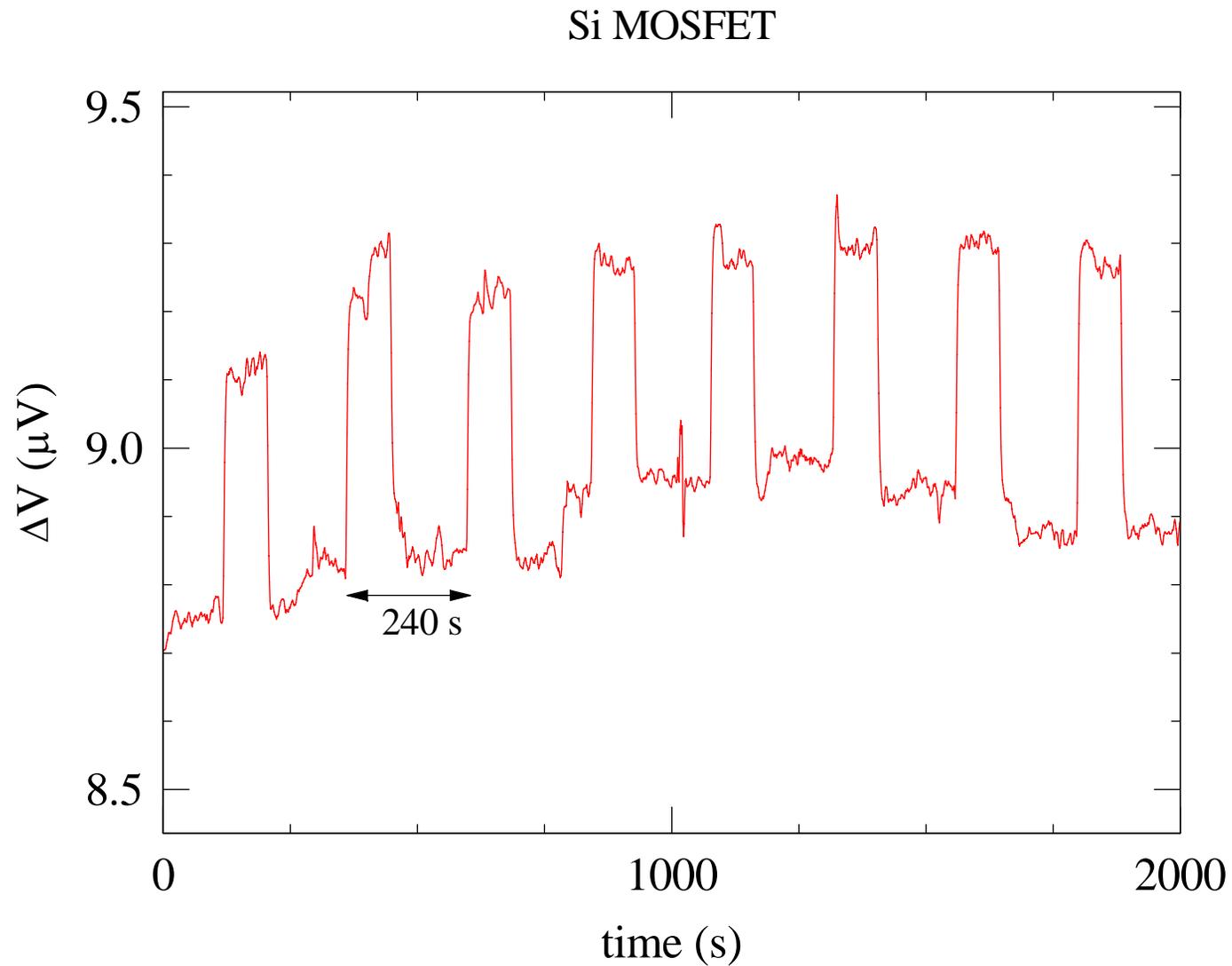
HF not only interfere with HF measurements as NMR but also sneaks to cryostats heating samples in the mK range, and dephasing electrons

Figure 3



almost the same spectrum everywhere  
+ computers, monitors etc

“4 min” switching due to e-microscope chiller  
(local C-120 problem solved)



# Diagnostic: Noise crash cart

The ability to measure and log noise problems whenever they arise



- Megger ground meter for ground loop detection and ground resistance meas.)
- Tektronix oscilloscope with FFT
- AC current clamp (ground loop current detection and spectroscopy
- DC current clamp
- Differential preamp, voltage probe
- Protek 3290 RF Spectrum Analyzer 0.1-2900MHz
- Laptop all can run on batteries
- isolation transformer

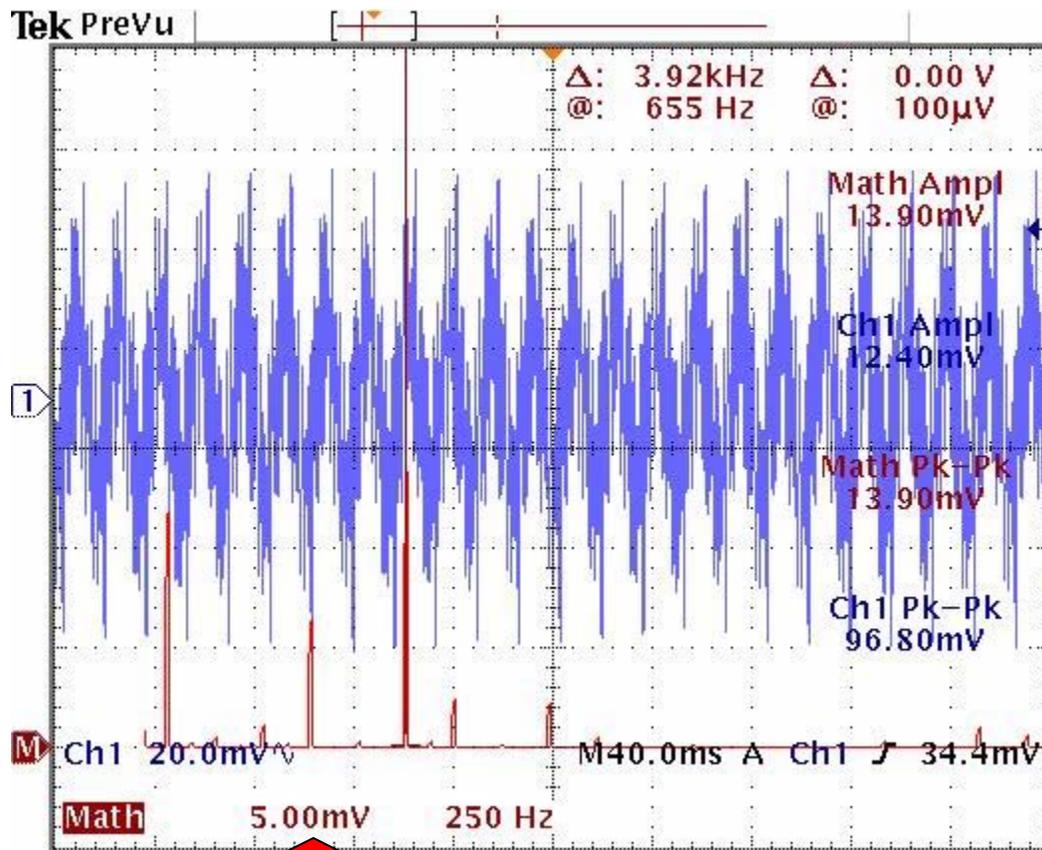


Quick detection of ground loops:  
current should be zero!



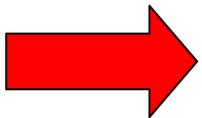
# Ground current measurements and spectra in grounding cables, pumping lines

Very bad, strong 60 and 660 Hz

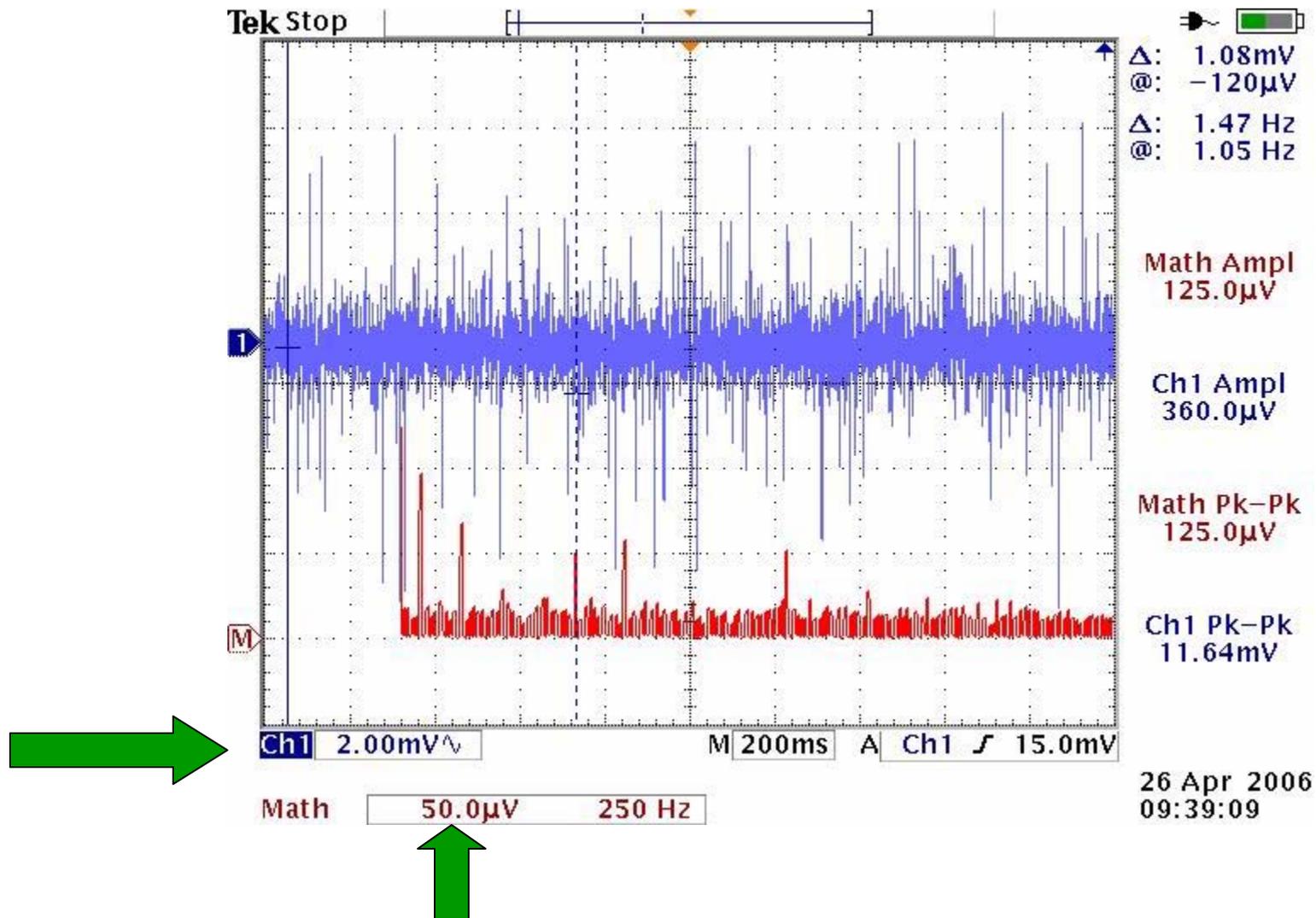


to isolation transf.

- Edit Math Definition
- Set FFT Source to Ch1
- Set FFT Vert Scale to Linear RMS
- Set FFT Window to Hanning



# Good, residual 60 Hz and harmonics



## Noise Crash Cart (NCC)

S. Hannahs, J. Jaroszynski, A. Migliori, T. Murphy, E. Palm

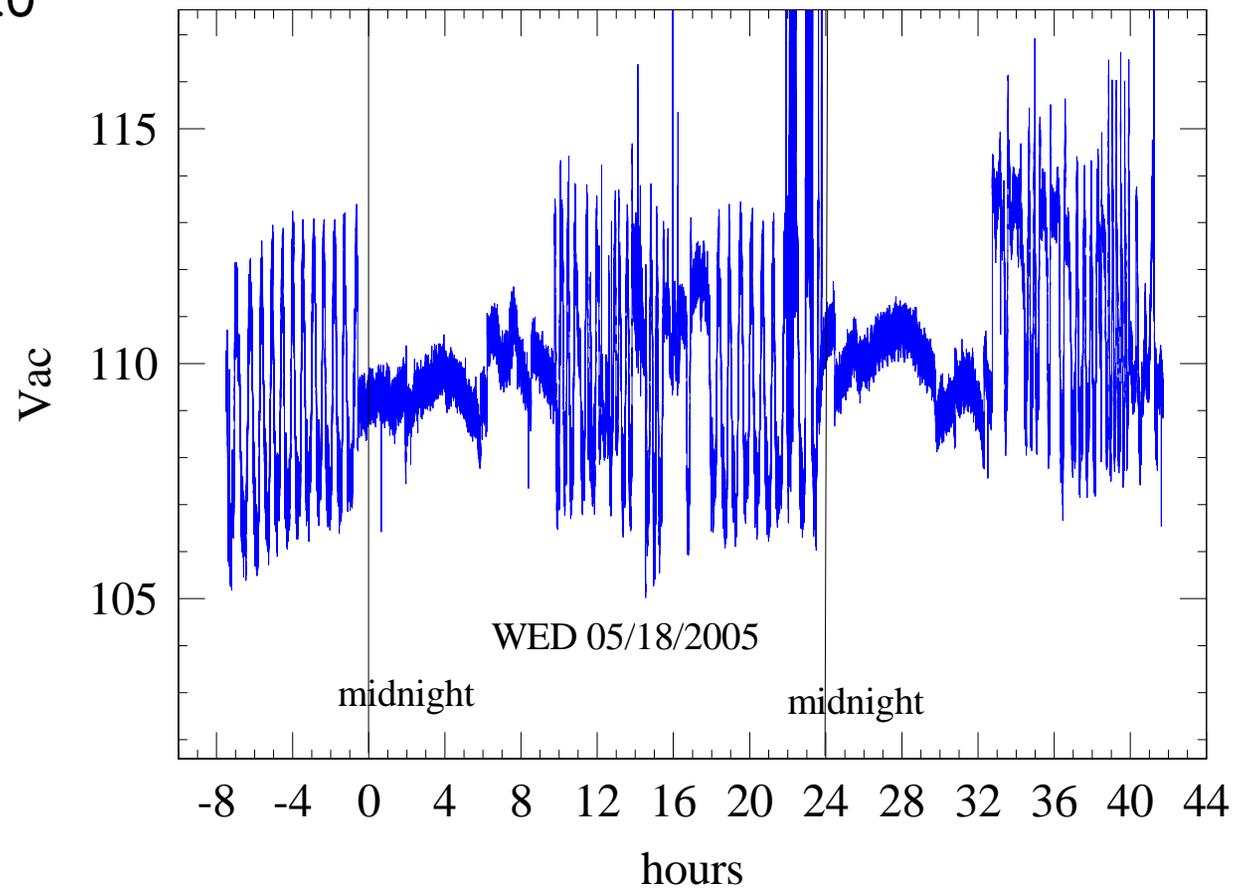
We describe here a “noise crash cart” (NCC, photo below). The NCC will provide a portable system able to respond to an obvious need to quantify noise in magnet measurement systems. Without the ability to quantify, the expected incremental response of systems to noise-abatement strategies cannot be detected reliably—and we expect that almost all improvements to be made will be individually small—so it is important not to miss any opportunities for lack of testability. The NCC is comprised of a portable isolation transformer, digital phosphor oscilloscope with Ethernet porting of data and a spectrum analyzer function built in (FFT) for making quantitative measurements, clamp-on current probes for measuring ground currents, and especially important to the mK facility, a RF signal strength analyzer. With this system we can measure and log ground noise and ground-loop currents, magnet power supply noise and frequency components, transmissions from the ELF (Navy) through cellular phone (893MHz to 1990MHz) and correlate these with noise in a measurement.

Item	Cost for each NCC
Tektronix TDS 3012B DPO scope with FFT and TDS3BATB battery pack, differential preamp	4.5K
Sola MCR 63-13-210-6 Isolation transformer	0.9K
AEMC MN 312 AC Current Clamp DC current gun	0.54K
Protek 3290 RF Signal Strength Analyzer 0.1-2900MHz	2.2K
Cables, cart and connectors	0.4K
Laptop and USB-RS-232 adapter	1.7K
Megger ground meter	1.4K

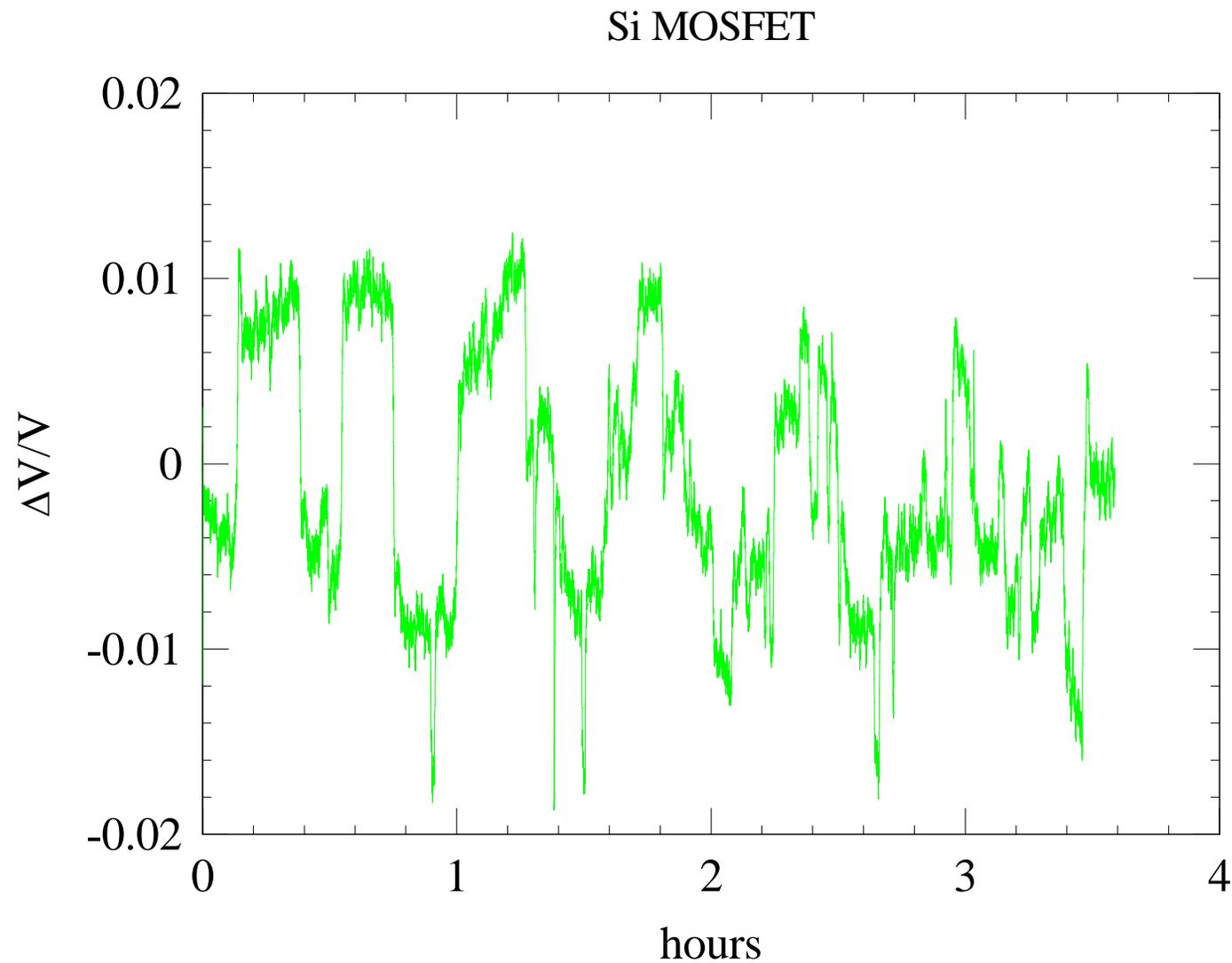
# Fighting the noise

Yet another problem:  
Changes of Vac from power line due to sweeps in resistive magnets

as seen in C-120



Sometimes these Vac fluctuations influence measurements  
(here V was is measured by lockin @ 10 $\mu$ V range)

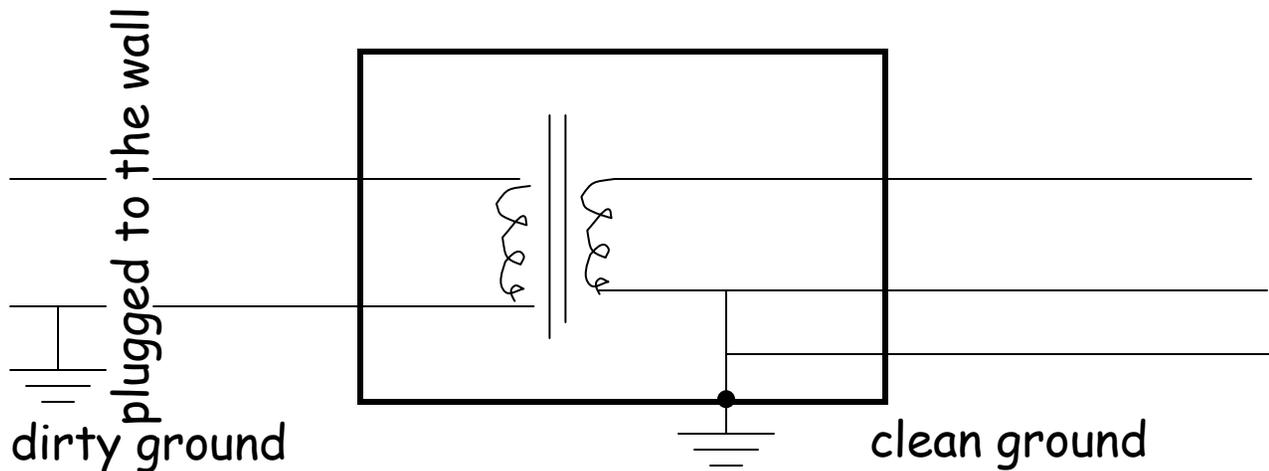


To stabilize V:  
ferro-resonant line-voltage regulators

they serve also as isolation transformers  
providing clean power and clean ground  
for experiment



to exp. set up



to exp. set up

# GPIB opto-isolators:

to cut ground loop between the computer and the experimental setup  
to reduce HF in mK experiment



B: clean side

A: dirty side

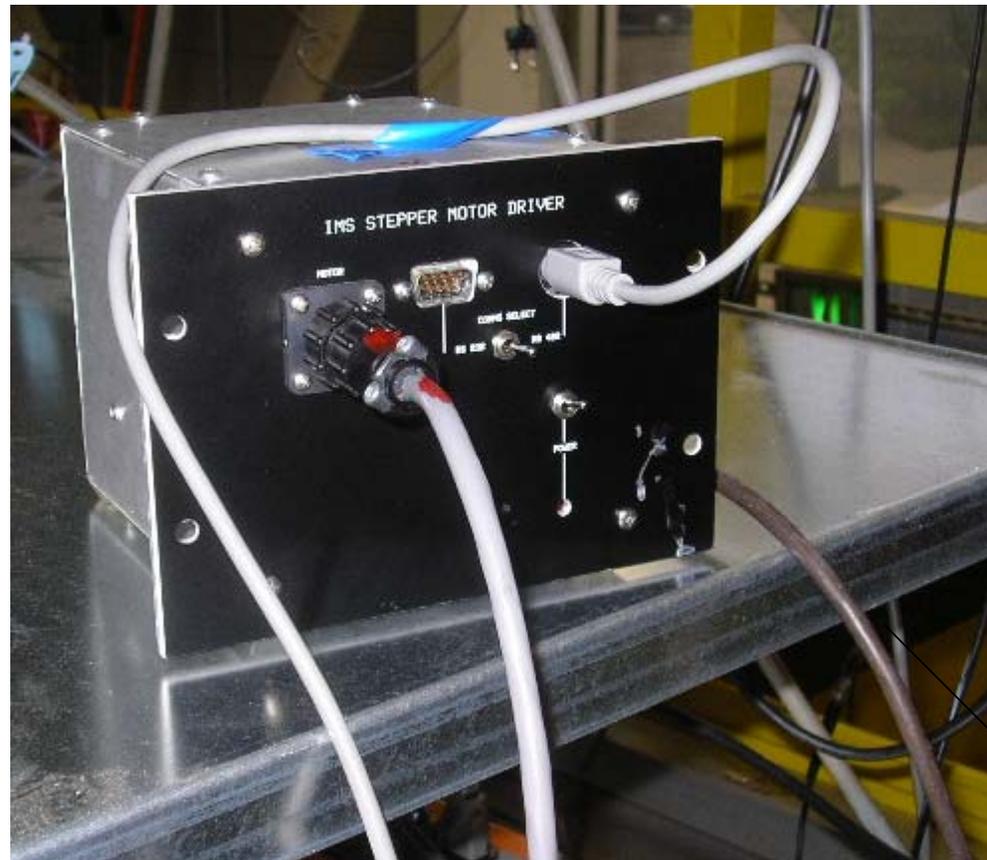


plugged into  
the wall outlet

←  
experiment

→  
computer

Important: plug into dirty ground other instruments which are connected to the computer via USB, RS etc. or isolate their ground

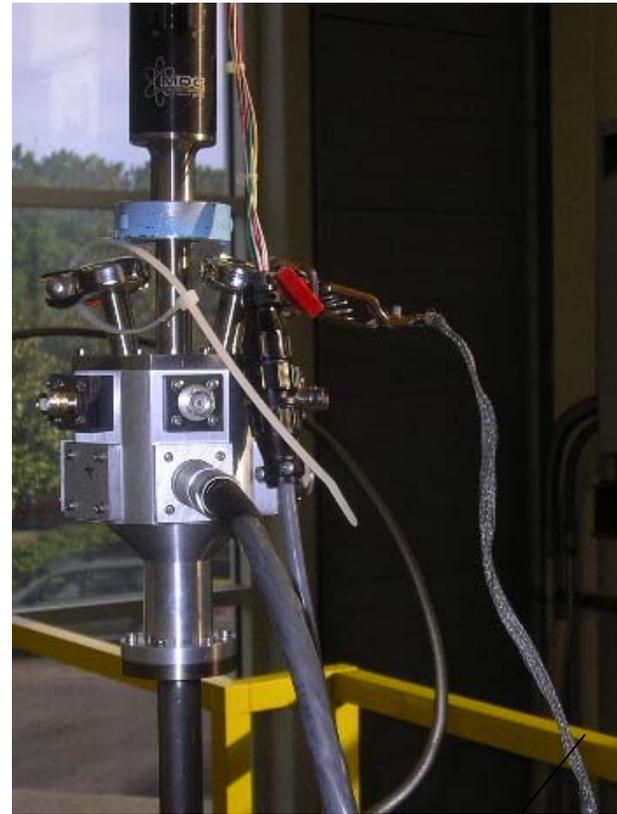


stepper motor driver

to the wall

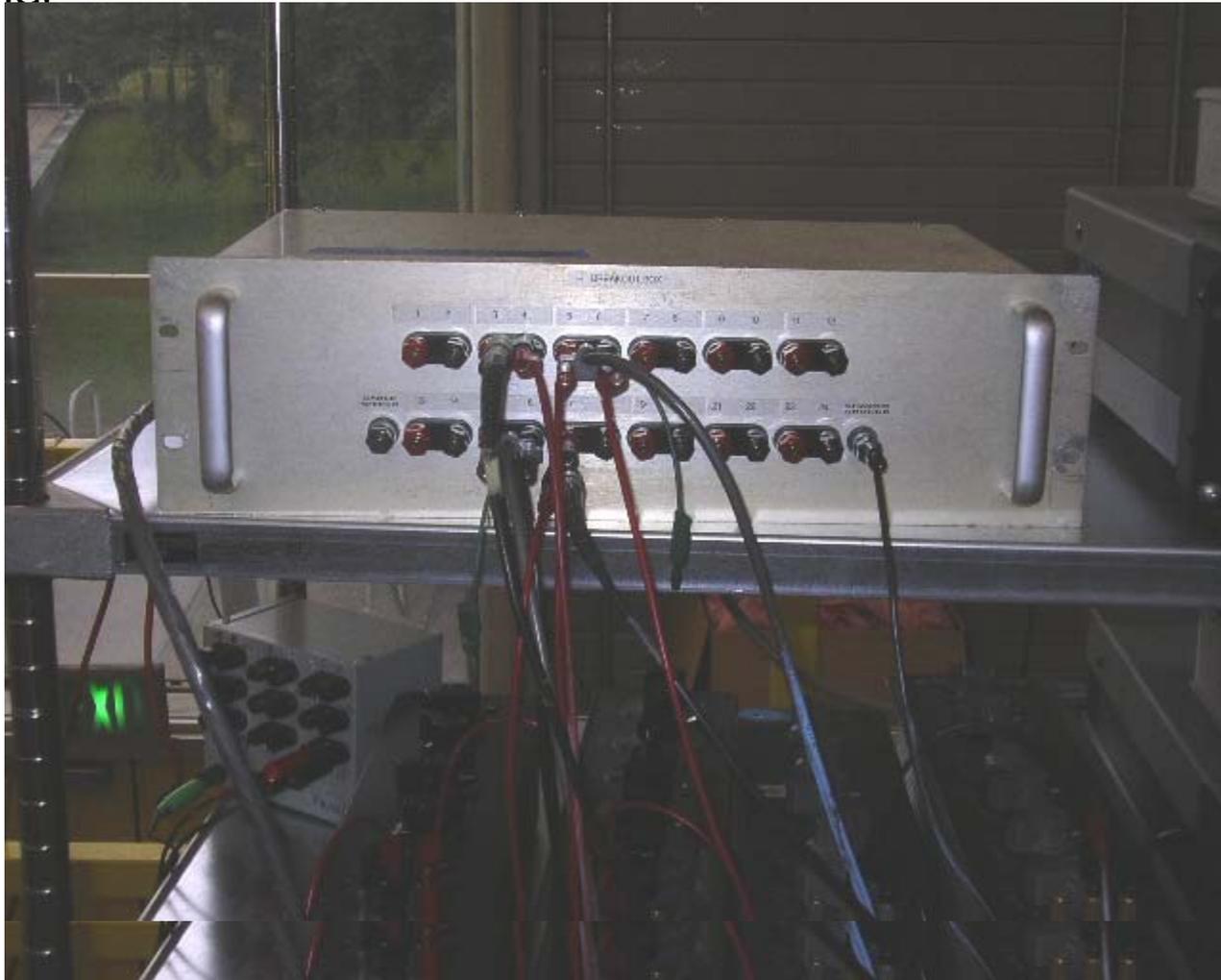


Important exception:  
in SC magnets do not isolate sliding probes  
Just opposite: ground them



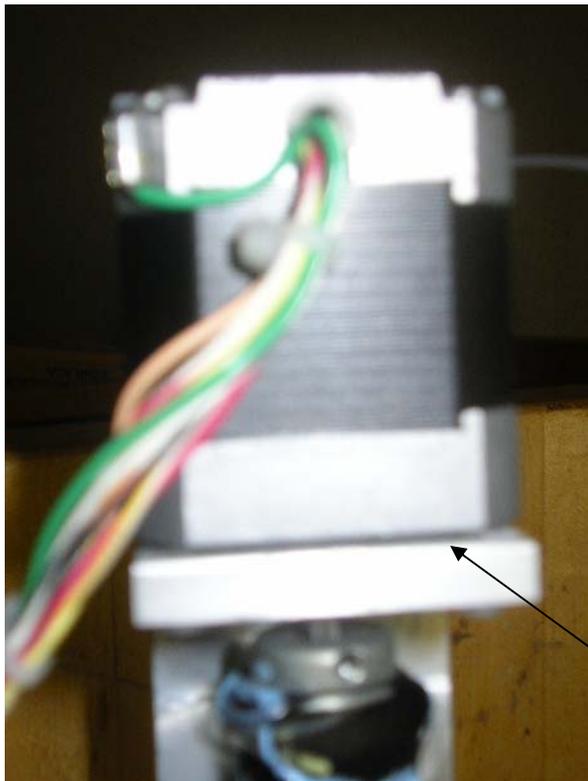
ground

Keep control on if possible noisy ground loops  
on the new SS instrumentation carts  
bad example:



Sometimes ground loop arises very unexpectedly:

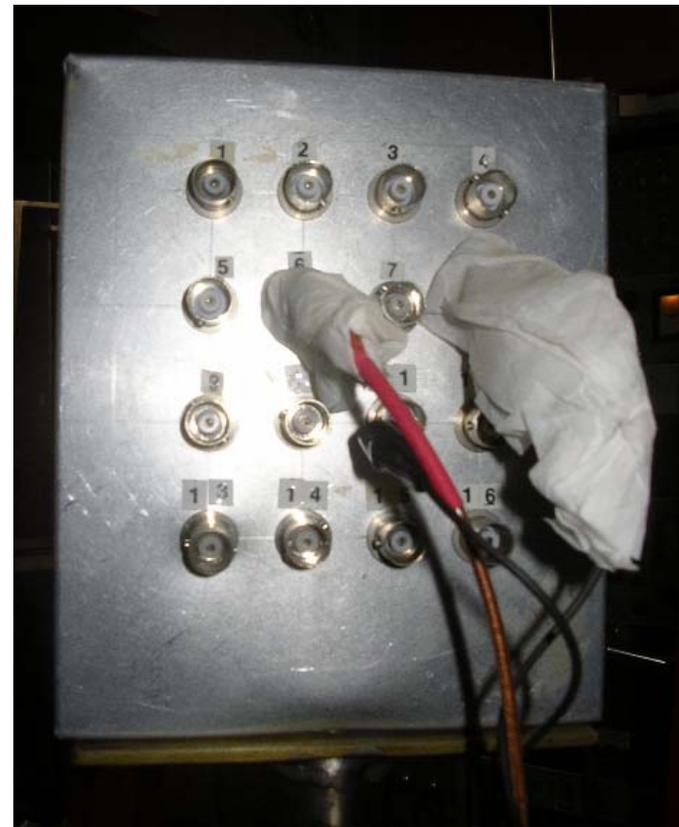
manufacturer fault:  
random connection between SR830  
chassis and transformer cover



dirt between stepper motor  
and the probe connects  
dirt computer to the clean experiment

## Thermoelectric effects (DC measurements only)

Cu/CuO could give as much as 1 mV/deg  
Thermally isolate terminals esp. when  
LN2 vapors from the cryostat  
Noise reduction down to nV possible



electrometer

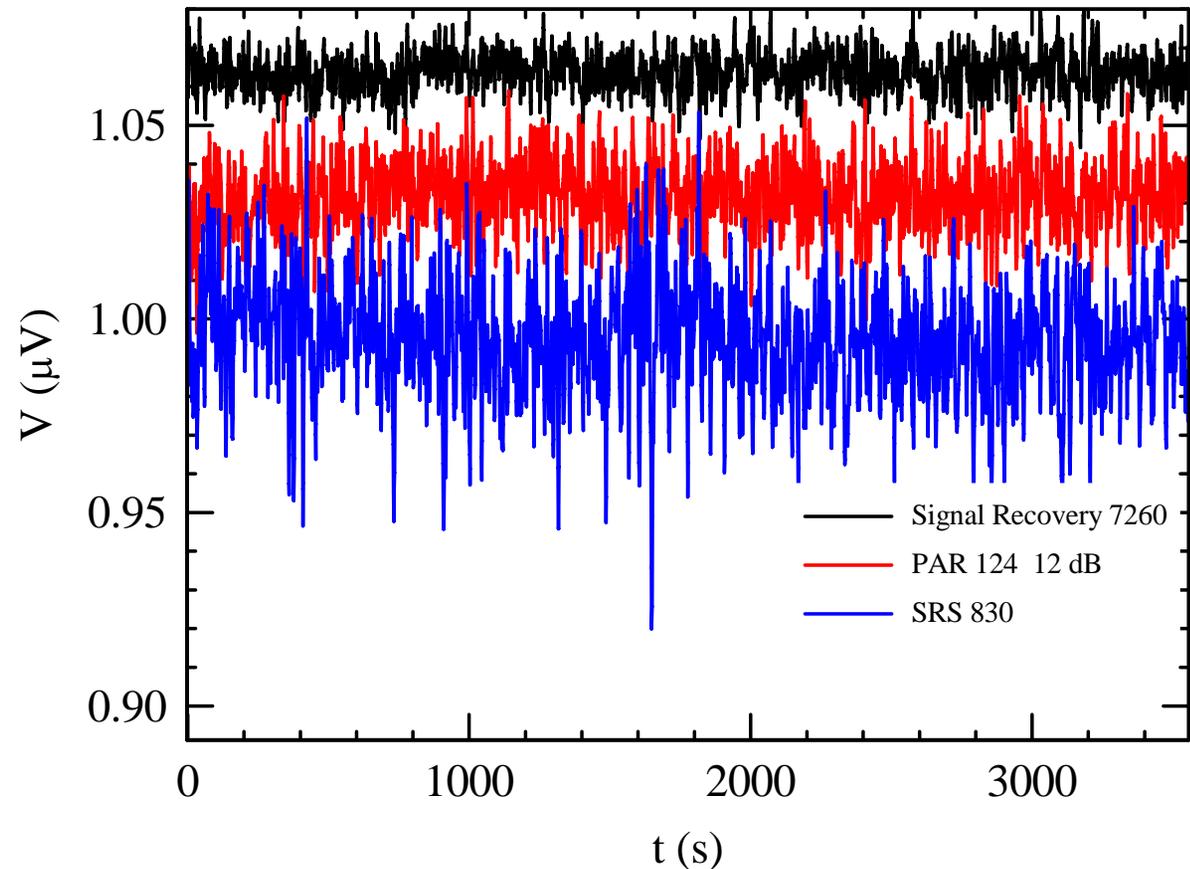
To reduce vibrations from pumping lines



Yet another source of noise and heating/cooling in the mK range:  
II type superconductors as a soldering alloy SnPb  
Excess heat when sweeping field up from  $B=0$

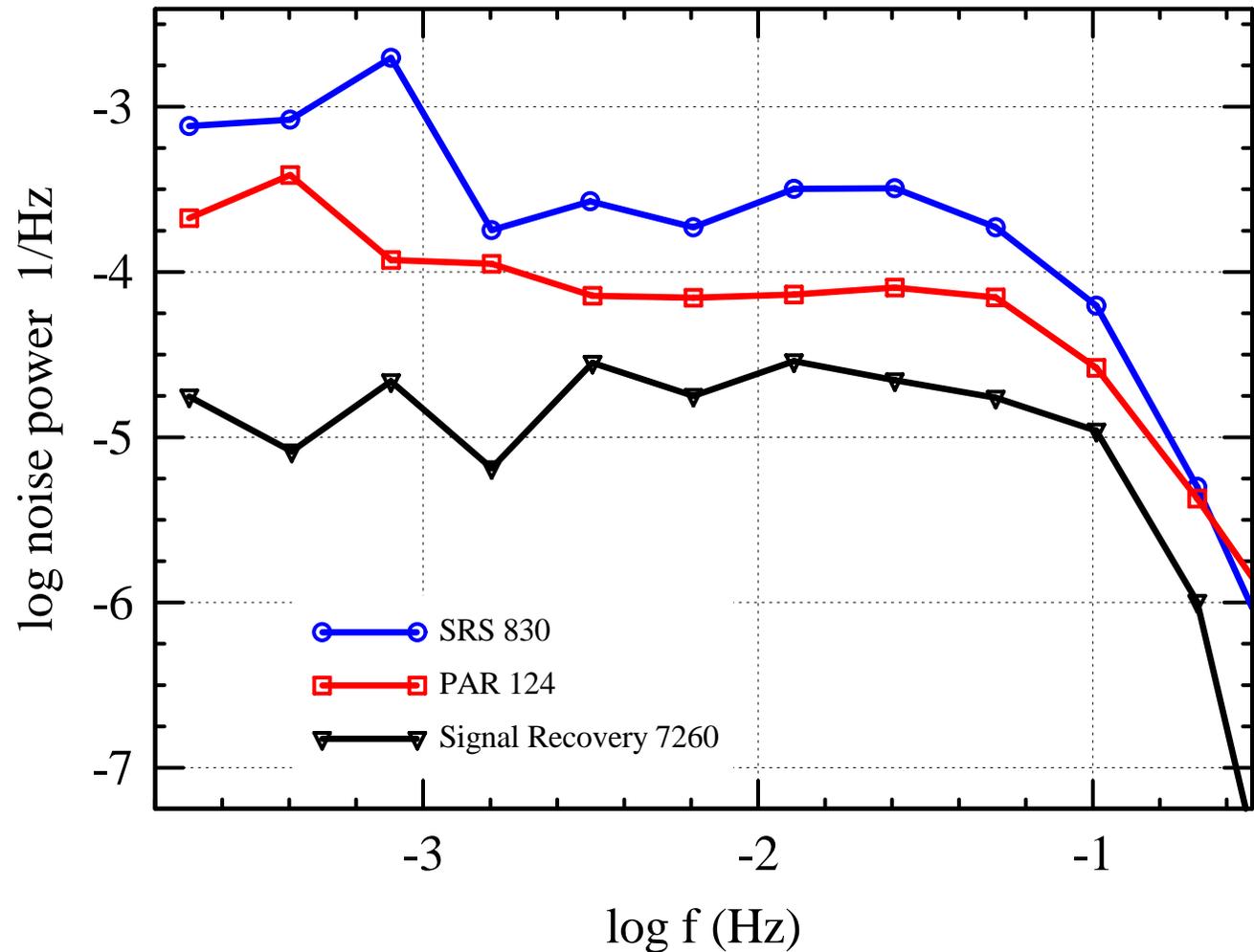
Solution: In, silver paste where possible

## Search for better lockins: Signal Recovery 7280 tested



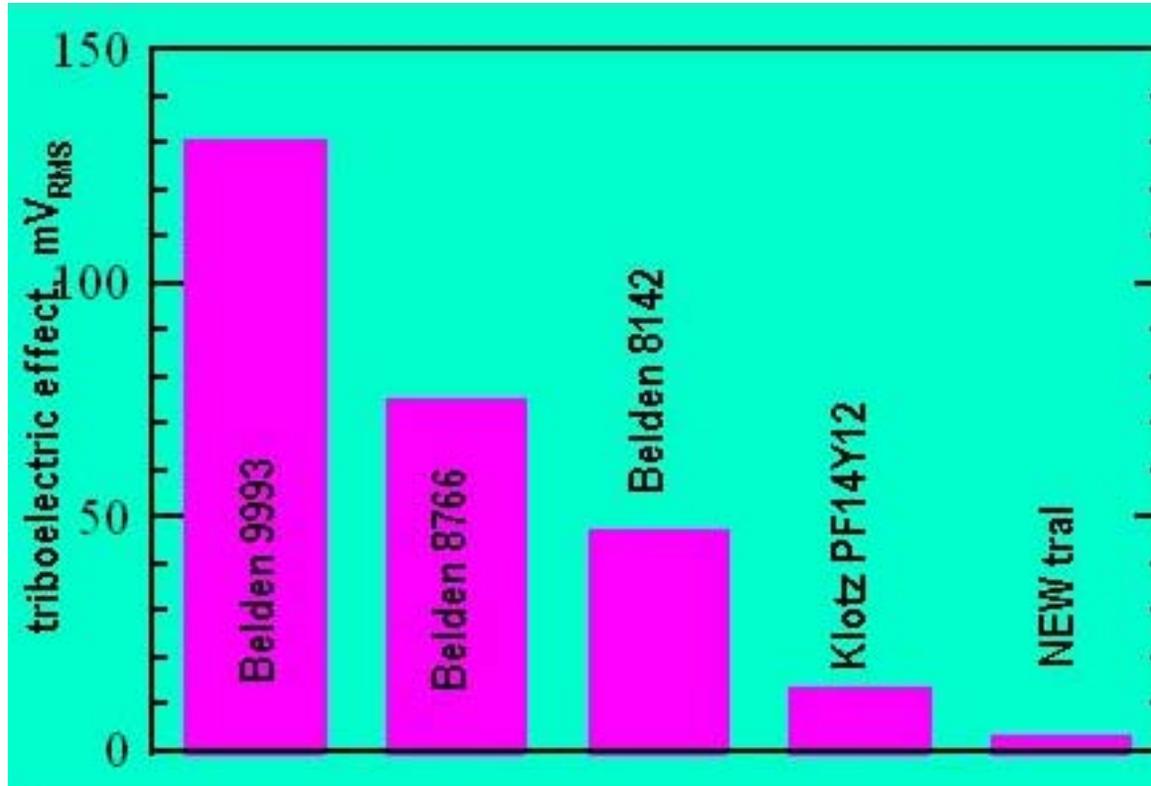
V vs. time, 1 nA on 1 kOhm metal film resistor  
time constant 1 s  $f=7$  Hz,  $V_{\text{RMS}}=5, 9,$  and 15 nV for  
Signal Recovery 7280, PAR 124 and SRS 830, respectively

Power spectra, averaged over octaves  
almost 2 orders of magnitude difference between SRS 830  
and Signal Recovery 7280 in a longtime (1h) stability

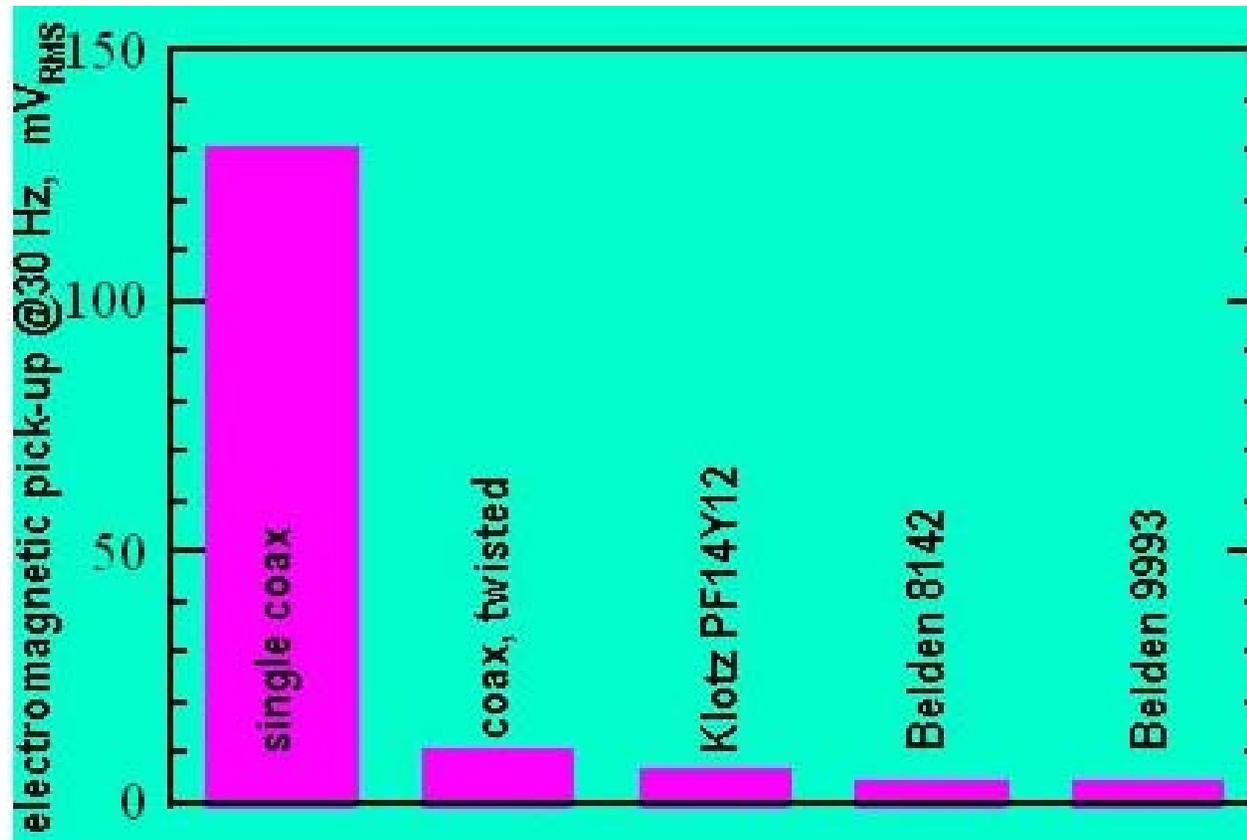




## Triboelectricity: results



## Electromagnetic pick up @ 33 Hz

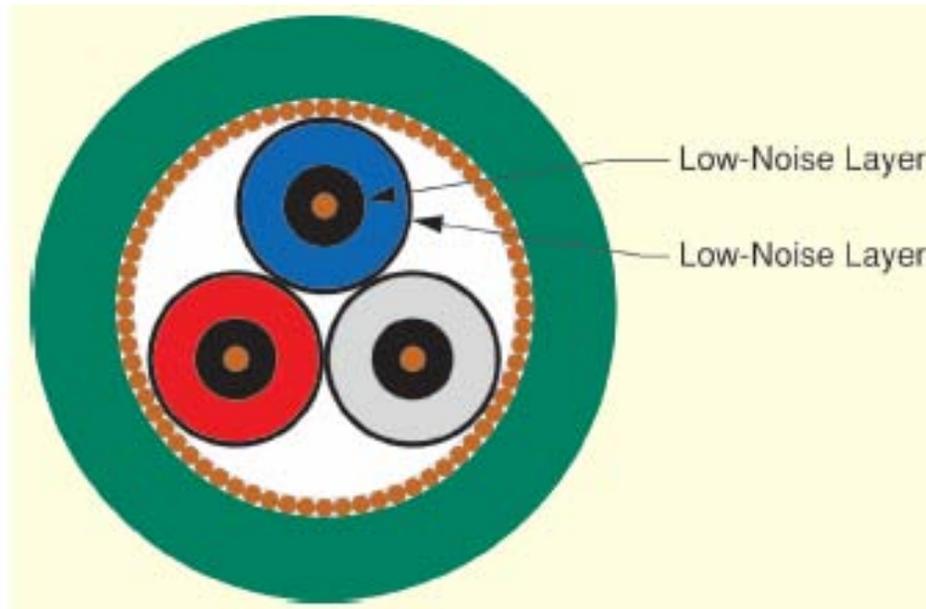


results for twisted pairs

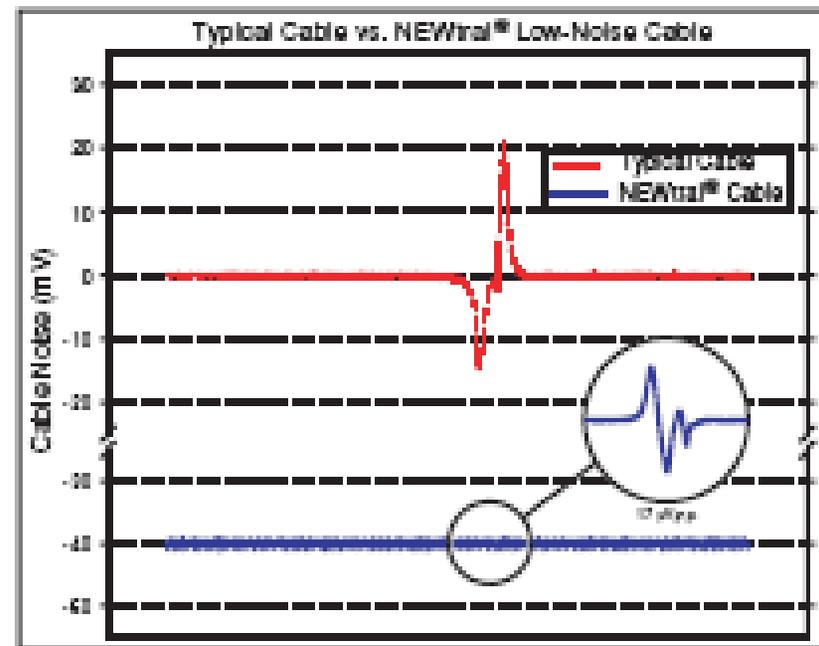
however an order of magnitude stronger between wires from different pairs!

try to avoid them mounting the sample!!!

Solution: new, very quiet cables from NEW  
(we already have their coaxes)

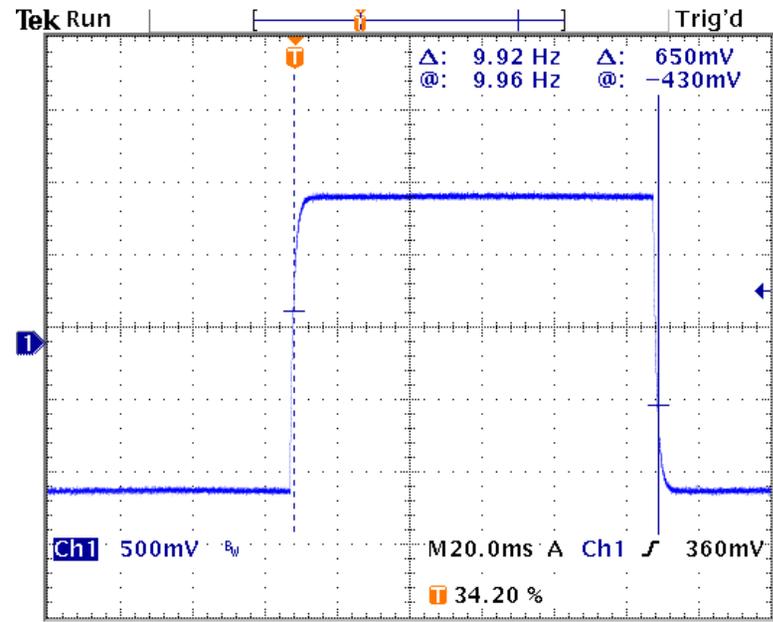
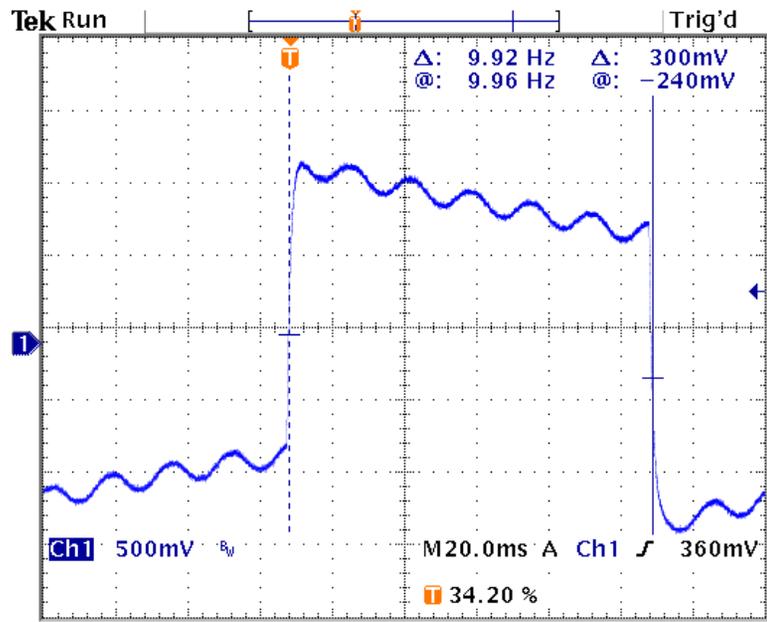


# NEWtral



## Examples: better T stabilization

### Lakeshore control heater/thermometer noise before and after proper grounding



Control thermometer waveform before connecting current-source shield on Lakeshore temperature controller and platform thermometer current source shields to racetrack ground, and replacing coax with twisted pair.

After—from 500mK fluctuations to sub mK temperature stability

S. Riggs, A. Migliori et al.

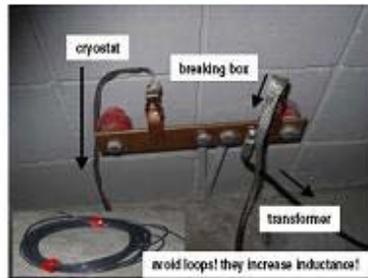
# Avoiding grounding/noise problems\*

The following items are critical to obtaining an optimum grounding system, otherwise ground loops would pick-up substantial interference from transformers and magnet power supplies (60 Hz, 720 Hz and harmonics)

Vibration isolate cryostat from magnet with rigid support & cryostat XYZ tilt. Isolate the cryostat or the probe from the magnet and from pumping lines. Use plastic clamps/o-rings. Check with multimeter that resistance between cryostat and magnet is high (before grounding cryostat)



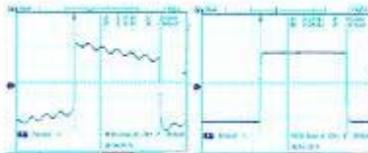
Ensure that isolation transformer is grounded, otherwise high floating voltage will be present on its chassis and the instruments. Power all the instrumentation (but computer and GPIB isolator) from isolation transformer. Ground the cryostat and breaking box at the same ground bar. Use twisted pair with shield, avoid coax cables. Ensure that shields of all the cables are grounded only on one side, usually on the breaking box.



Isolate GPIB bus ground using National Instruments GPIB-120A isolator. Use "noise crash cart" to check if you have proper grounding without loops.



Proper grounding reduces unwanted noise dramatically and improves temperature stability. Example: temperature controller waveforms before and after proper grounding correspond to improvement from 500 mK to sub mK temperature stability.



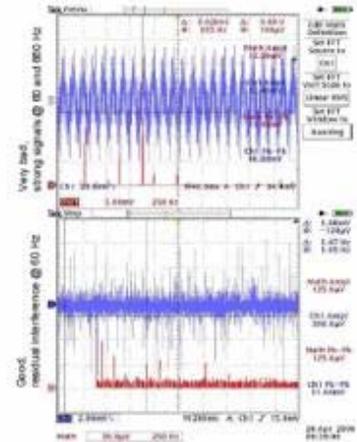
\* in case of grounding/noise issues contact Jan Jaroszyński 644 1175 jaroszy@magnet.fsu.edu

## Noise crash cart

To quick check your setup you may use one of the noise crash carts, usually located in cell #7 or instrumentation storage room



Put clamp on the grounding cable of isolation transformer (or cryostat) and connect it to the oscilloscope. Set the scope to, say, 200 ms/div, 1 mV/div. If signal looks as a white noise with amplitude < few millivolts, your set-up is properly grounded. For spectral analysis switch on FFT option: [MATH], [FFT]. If ground loops are absent, almost flat FFT would be seen. Otherwise several characteristic frequencies show up: 60 Hz (power lines, transformers), 720±60 Hz (magnet DC power supply if on) and their harmonics. Still, if their amplitude is less than a few hundreds microvolts (1µV corresponds to 10µA ground current) it is probably a result of capacitive pick-up, not bad ground. Additionally you could see  $f \approx 8$  Hz, 20 kHz, 500 kHz, 1.27 MHz, ~ 20 MHz, broad band from FM radio and TV. These frequencies should be avoided in measurements.



To spot sources of high frequency in the range 100 kHz - 2.9 GHz other than listed (for instance some UPSs, computers) above you may use Protek 100kHz-2.9GHz RF Signal Strength Analyzer. Set the center frequency (e.g. set 100 [CTR], [ENTER]). Then select the step. Measured spectra consist of 160 steps: e.g. [F2], set 1 MHz, [ENTER], and [F1] for run. Protek will scan from 20 to 180 MHz.

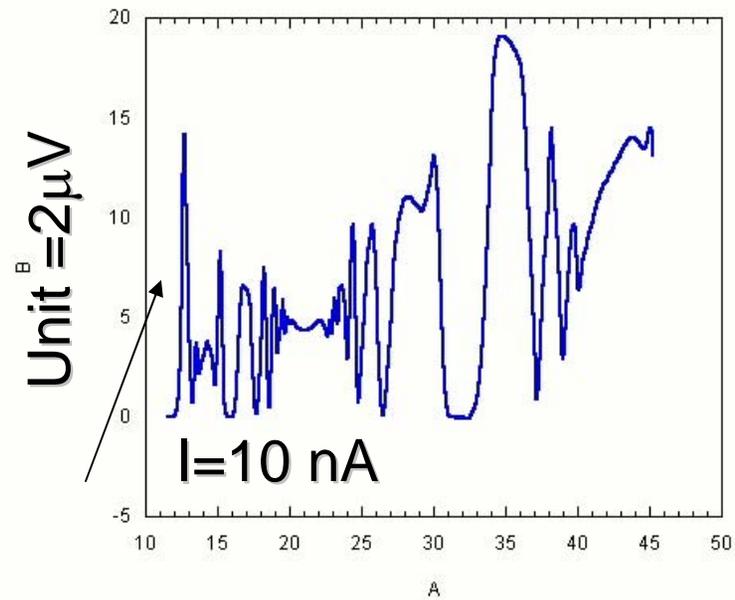
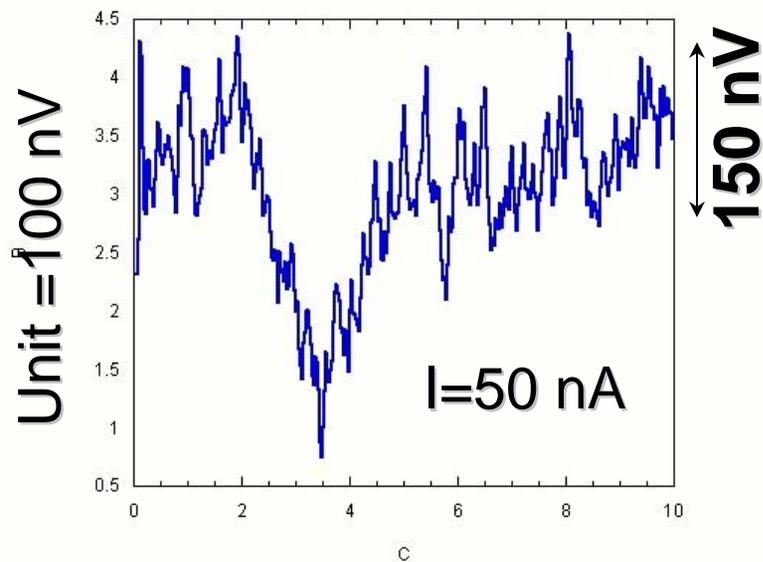


On noise crash carts you could also find clamp-on Hall probe to measure DC current in ground cables, voltage probes and preamplifiers to analyze signals in your circuit, and laptops for data taking. Importantly, all these instruments could be powered from batteries which makes it possible to avoid interference from their power lines.



## Examples

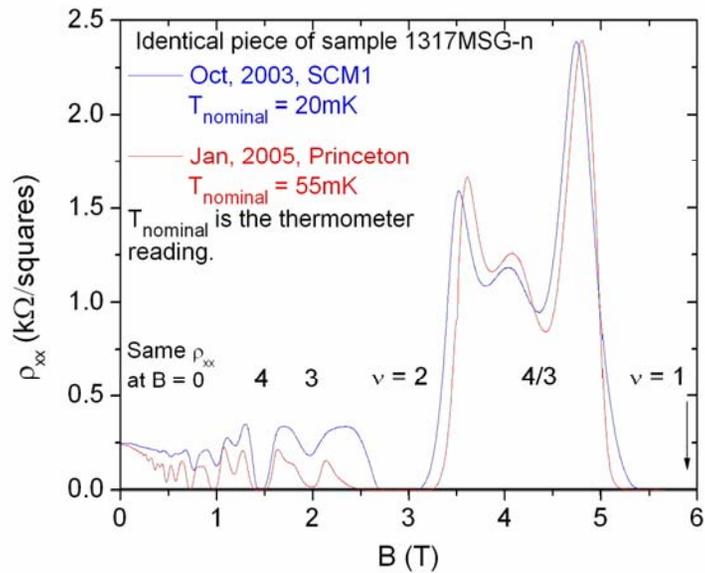
Noise @ 50 nA  $150 \text{ nV p-p}/10 \mu\text{V} = 1.5\%$



FQHE and RDNMR measurement in the hybrid (Jiang et al)  
after better grounding

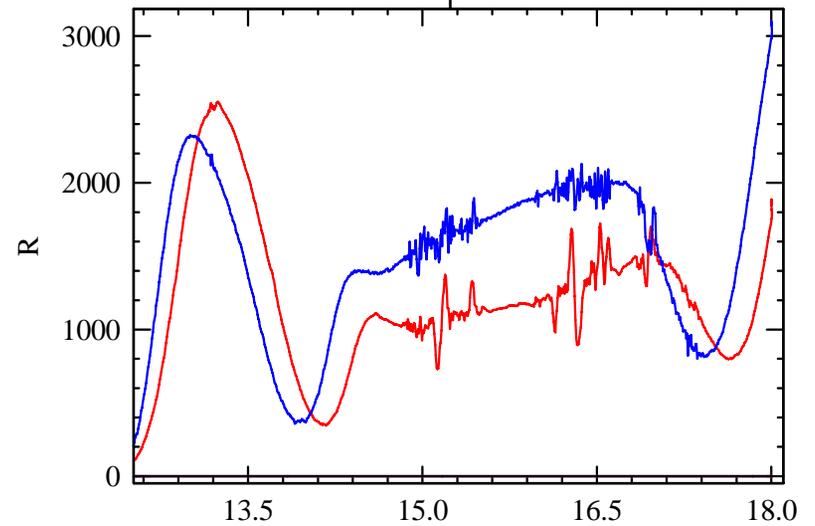
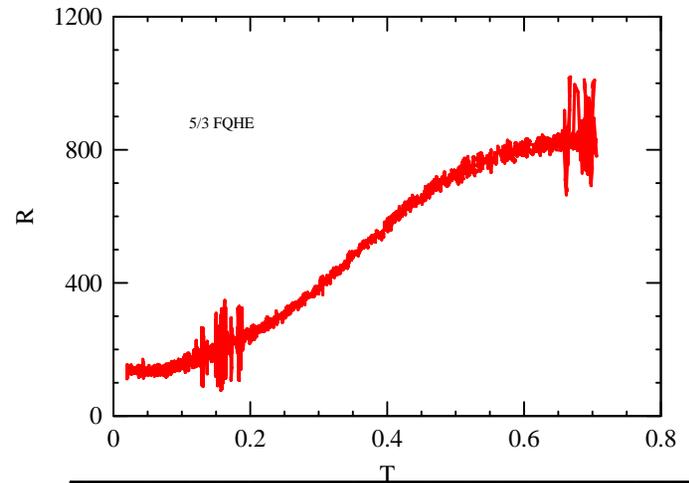
# Examples: SCM1 problems

## cooling problems?



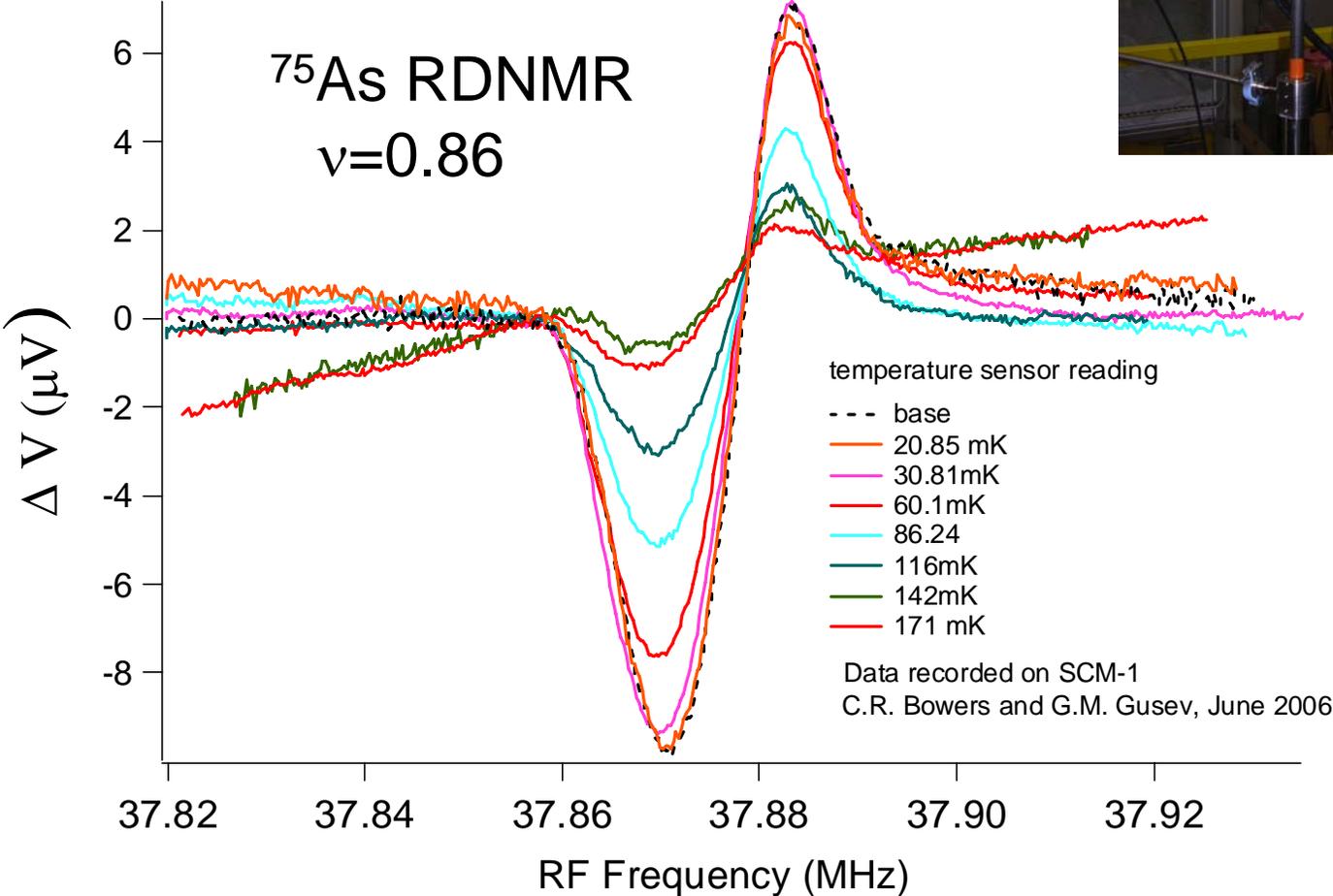
Keji Lai et al.

## cooling and noise problems



Nathaniel Bishop et al.

Recent improvement in SCM1: proper grounding,  
quiet cables, HF filters, better lockin  
10 days/nights long hard work of our guests:  
R. Bowers and G. Gusev



## Other issues, ideas

- high frequency interference in millikelvin bldg., hybrid which are elevated and probably constitute good resonance cavities for FM frequency which spoils NMR and other HF experiments  
solution: to shield windows with foil or mesh
- better lockins: Signal Recovery (former PAR, E&G etc) model 7280 tested, 7265 will be tested soon. Tests show 7280 is much better for sensitive measurements as RDNMR, noise measurements, etc
- purchase small accessories as DC ground breakers for coaxes ferrite clamp on, clamp on ground resistance meter for quick tests, zippered cable shielding to reduce HF, electrostatic, vibration
- preamps closer to experiment (cryogenic?)
- “universal” breaking boxes

